

Application of Sign Depth to Point Process Models

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Load Sharing & Damage Accumulation

- In a **load sharing system**, the failure of one component affects the performance of the remaining components.
 - ↔ Whenever a tension wire breaks, the load is redistributed among the remaining wires.
 - ↔ The risk of another failure increases.
 - ↔ The failure risk depends on the *number* of remaining components.
- If the failure risk also depends on *how long* the components were exposed to the load, the system is subject to **damage accumulation**.



Figure: Broken tension wires.

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Notation Used in This Talk

- In a system with $I \in \mathbb{N}$ components, we denote the random failure times by

$$0 < T_1 < T_2 < \dots < T_I, \quad \text{and } T_i = \infty \text{ for } i > I.$$

- We denote the corresponding realizations by t_1, \dots, t_I , so that $T_i(\omega) = t_i$ ($i \in \mathbb{N}$).
- The counting process $N = (N_t)_{t \geq 0}$ counts the failures up to the time $t \geq 0$,

$$N_t := \sum_{i=1}^{\infty} \mathbb{1}_{(0,t]}(T_i).$$

- For each $j \in \mathbb{N}$ we consider an independent copy of this system:
 - The counting processes $N^{(j)}$, $j \in \mathbb{N}$, are i.i.d. copies of N .
 - Similarly, let $(T_i^{(j)})_{i \in \mathbb{N}}$ denote the point process associated with $N^{(j)}$.

Approach for an intensity-based model:

Identify the failure risk of the components in system j with the stochastic intensity of the counting process $N^{(j)}$.

Hazard Function & Stochastic Intensity

- The *conditional hazard function* h_i of $T_i^{(j)}$ given $T_1^{(j)} = t_1^{(j)}, \dots, T_{i-1}^{(j)} = t_{i-1}^{(j)}$ is

conditional
density function

conditional
survival function

$$h_i(t | t_1^{(j)}, \dots, t_{i-1}^{(j)}) = \frac{f_i(t | t_1^{(j)}, \dots, t_{i-1}^{(j)})}{S_i(t | t_1^{(j)}, \dots, t_{i-1}^{(j)})}.$$

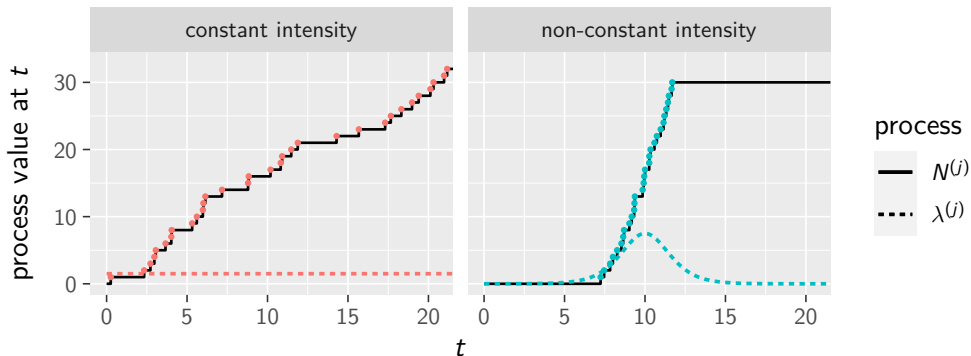
- The *stochastic intensity* $\lambda^{(j)}$ of the counting process $N^{(j)}$ is then piecewise defined by

$$\lambda^{(j)}(t) := \begin{cases} h_1(t), & 0 \leq t \leq t_1^{(j)}, \\ h_i(t | t_1^{(j)}, \dots, t_{i-1}^{(j)}), & t_{i-1}^{(j)} < t \leq t_i^{(j)}, i \geq 2. \end{cases}$$

- $\lambda^{(j)}$ constitutes the instantaneous component failure rate of the j th system, that is,

$$\lambda_t^{(j)} dt = \mathbb{E} \left[N^{(j)}(dt) | \sigma(\{N_s^{(j)} : s < t\}) \right] = \mathbb{P} \left[N^{(j)}(dt) = 1 | \sigma(\{N_s^{(j)} : s < t\}) \right].$$

Parametric Intensity-Based Point Process Model



Parametric intensity-based point process model

Let $\theta \in \Theta$ be the parameter of interest, where $\Theta \subset \mathbb{R}^d$, $d \in \mathbb{N}$. An intensity-based point process model is given by a parametric class of intensities,

$$\mathcal{M} = \{\lambda_\theta : \theta \in \Theta\}.$$

We assume the following:

- \mathcal{M} contains the true intensity λ of N .
- There is a *true* $\theta^* \in \Theta$ such that $\lambda = \lambda_{\theta^*}$.

Basquin Load Sharing Model With Damage Accumulation

$$\lambda_{\theta}^{(j)}(t) := \theta_1 \left(s_j \frac{I}{I - N_{t^-}^{(j)}} \right)^{\theta_2} A_j(t)^{\theta_3} \mathbb{1}_{\{N_{t^-}^{(j)} < c_j\}} .$$

Figure: Schematic of the Basquin load sharing model with damage accumulation (cf. Basquin 1910, based on Müller and Meyer 2022).

For each $j \in \mathbb{N}$, the damage accumulation term A_j is defined as:

$$A_j(t) = \int_0^t s_j \frac{I}{I - N_{u^-}^{(j)}} du .$$

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j th system

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model parameter
 $\theta = (\theta_1, \theta_2, \theta_3)^\top$

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$$\lambda^{(j)}_{\theta}(t) := \theta_1 \left(\underbrace{s_j \frac{I}{I - N_{t^-}^{(j)}}}_{\text{load sharing term}} \right)^{\theta_2} A_j(t)^{\theta_3} \mathbb{1}_{\{N_{t^-}^{(j)} < c_j\}} .$$

model parameter $\theta = (\theta_1, \theta_2, \theta_3)^{\top}$

I = total number of components.

$N_{t^-}^{(j)}$ = # of failed components before time t .

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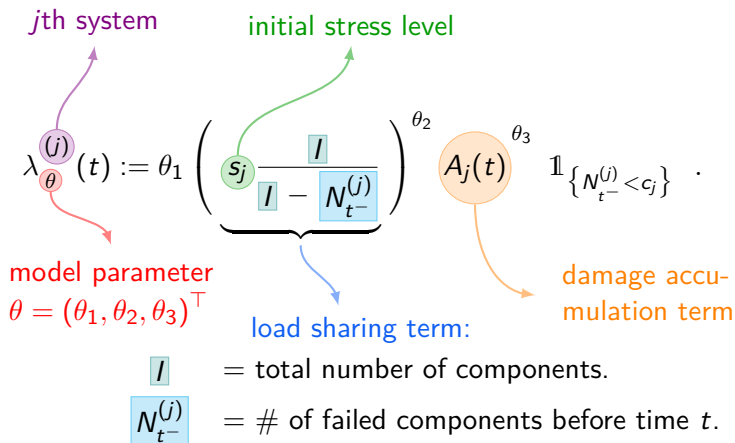


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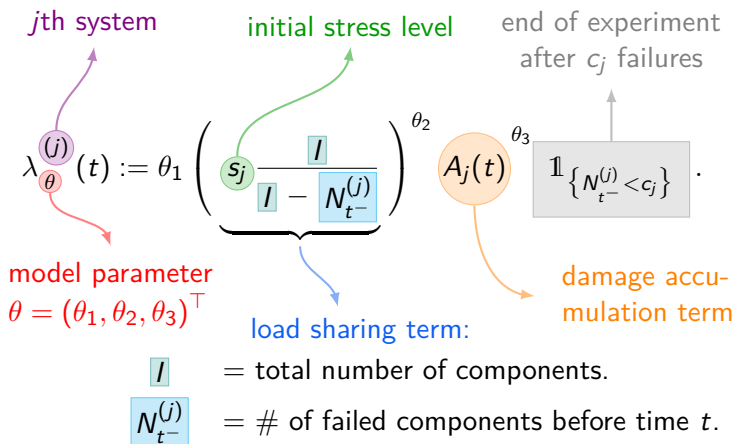


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The K -Sign Depth

Definition (K -sign depth Leckey et al. 2023)

For Residuals $R_n = R_n(\theta)$, the K -sign depth is defined as

$$d_K(R_1, \dots, R_N) := \frac{1}{\binom{N}{K}} \sum_{1 \leq i_1 < \dots < i_K \leq N} \mathbb{1}_{\{(R_{i_1}, \dots, R_{i_K}) \in \mathcal{A}\}}.$$

where \mathcal{A} is the set of K -tuples with alternating signs, that is,

$$\mathcal{A} := \left\{ (x_1, \dots, x_K) \in \mathbb{R}^K : x_i \cdot x_{i-1} < 0 \text{ for all } i = 2, \dots, K \right\}.$$

Definition (3-sign depth test for arbitrary hypotheses)

A level $\alpha \in (0, 1)$ test for $\mathcal{H}_0 : \theta^* \in \Theta_0 \subset \Theta$ is given via:

$$\text{Reject } \mathcal{H}_0 \text{ if } \sup_{\theta \in \Theta_0} N \left(d_3(R_1(\theta), \dots, R_N(\theta)) - \frac{1}{4} \right) < q_\alpha,$$

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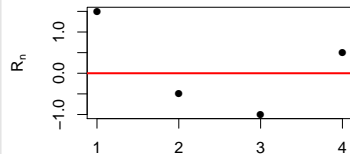
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Example: Let $K = 3$, $N = 4$,
 $(r_1, \dots, r_4) = (1.5, -0.5, -1, 0.5)$.



	n	
alternating	:	not altern.
0	:	0

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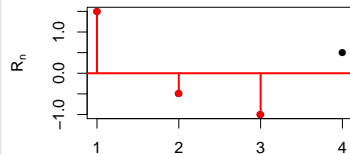
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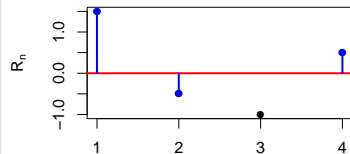
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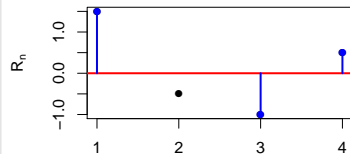
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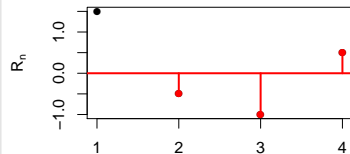
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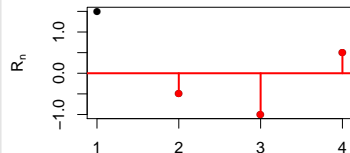
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$$d_3(r_1, \dots, r_4) = \frac{2}{2+2}$$

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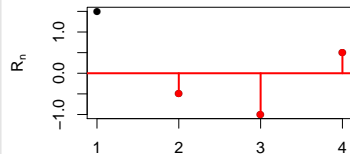
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$$d_3(r_1, \dots, r_4) = \frac{2}{2+2}$$

(K1) $R_1(\theta^*), \dots, R_N(\theta^*)$ are independent w.r.t. \mathbb{P}_{θ^*} .

(K2) $\mathbb{P}_{\theta^*}(R_n(\theta^*) > 0) = 1/2$ and $\mathbb{P}_{\theta^*}(R_n(\theta^*) < 0) = 1/2$.

The Hazard Transform

Definition (Hazard transform)

The hazard transform $\tilde{R}_{j,i}(\theta)$ of $T_i^{(j)}$ at $\theta \in \Theta$ is defined as

$$\tilde{R}_{j,i}(\theta) := H_i^\theta(T_i^{(j)} | T_1^{(j)}, \dots, T_{i-1}^{(j)}), \quad j \in \mathbb{N}, i = 1, \dots, c_j,$$

where the cumulative conditional hazard function is given by

$$H_i^\theta(t | T_1^{(j)}, \dots, T_{i-1}^{(j)}) := \int_{T_{i-1}^{(j)}}^t h_i^\theta(u | T_1^{(j)}, \dots, T_{i-1}^{(j)}) \, du.$$

At the true parameter θ^* holds: $\tilde{R}_{j,i}(\theta^*) \stackrel{\text{i.i.d.}}{\sim} \mathcal{E}(1)$.

Definition (Median-centred hazard transform)

The median-centred hazard transform $R_{j,i}(\theta)$ is defined as

$$R_{j,i}(\theta) := \tilde{R}_{j,i}(\theta) - \ln(2).$$

Reminder:

$$\mathcal{M} = \{\lambda_\theta : \theta \in \Theta\},$$

on $\{T_{i-1}^{(j)} < t \leq T_i^{(j)}\}$:

$$\lambda_\theta^{(j)}(t) = h_i^\theta(t | T_{1:(i-1)}^{(j)}).$$

Requirements for the 3-sign depth test:

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The transforms are independent.
 \Rightarrow (K1) is met.

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At the true parameter θ^* holds:

$$\tilde{R}_{j,i}(\theta^*) \stackrel{\text{i.i.d.}}{\sim} \mathcal{E}(1).$$

Reminder:

$$\mathcal{M} = \{\lambda_\theta : \theta \in \Theta\},$$

on $\{T_{i-1}^{(j)} < t \leq T_i^{(j)}\}$:

$$\lambda_\theta^{(j)}(t) = h_i^\theta(t | T_{1:(i-1)}^{(j)}).$$

Requirements for the 3-sign depth test:

The transforms are independent.
 \Rightarrow (K1) is met.

Definition (Median-centred hazard transform)

The median-centred hazard transform $R_{j,i}(\theta)$ is defined as

$$\text{med}(\tilde{R}_{j,i}(\theta^*)) = \ln(2)$$

$$R_{j,i}(\theta) := \tilde{R}_{j,i}(\theta) - \ln(2).$$

Transforms are median-centred.
 \Rightarrow (K2) is met.

The Hazard Transform

Definition (Hazard transform)

The hazard transform $\tilde{R}_{j,i}(\theta)$ of $T_i^{(j)}$ at $\theta \in \Theta$ is defined as

$$\tilde{R}_{j,i}(\theta) := H_i^\theta(T_i^{(j)} | T_1^{(j)}, \dots, T_{i-1}^{(j)}), \quad j \in \mathbb{N}, i = 1, \dots, c_j,$$

where the cumulative conditional hazard function is given by

$$H_i^\theta(t | T_1^{(j)}, \dots, T_{i-1}^{(j)}) := \int_{T_{i-1}^{(j)}}^t h_i^\theta(u | T_1^{(j)}, \dots, T_{i-1}^{(j)}) \, du.$$

At the true parameter θ^* holds:

$$\tilde{R}_{j,i}(\theta^*) \stackrel{\text{i.i.d.}}{\sim} \mathcal{E}(1).$$

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Requirements for the 3-sign depth test:

The transforms are independent.
 \Rightarrow (K1) is met.

Use 3-sign depth test.

Transforms are median-centred.
 \Rightarrow (K2) is met.

Robustness of the 3-Sign Depth Test

- In a simulation study, we compare the 3-sign depth test with two other methods:
 - Wald-type test based on a **minimum distance** estimator of Kopperschmidt and Stute 2013.
 - **Likelihood-ratio** test constructed from the Cox partial likelihood.
- To assess their robustness, we apply them to contaminated data.
- During the simulation of the data, a fixed proportion p of the data is contaminated:
 - 1 Determine which $\lfloor p \cdot c_j \rfloor$ waiting times of the j th system are contaminated.
 - 2 Randomly replace these waiting times with atypically small or large values.

	model parameter		covariates			# of processes
parameter/covariate	θ^*	l	c_j	p	s_j	J
chosen value(s)	$(10^{-4}, 3, 1)^\top$	25	10	0.4	80, 120, 200	9, 90

Table: The selected model parameters and values of covariates for the simulation study.

Robustness: Type I Errors for Contaminated Data

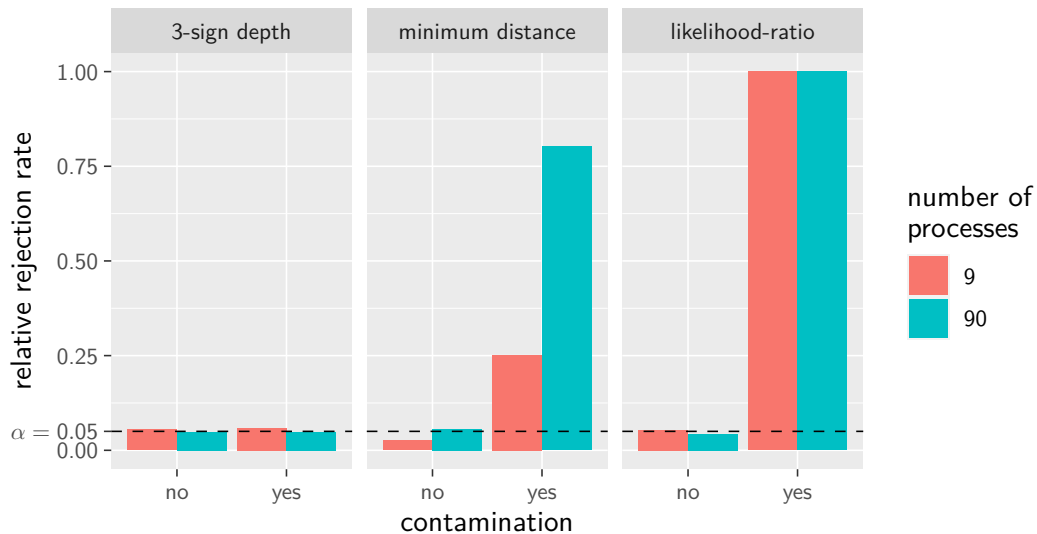


Figure: Type I errors of different level $\alpha = 0.05$ tests for $\mathcal{H}_0 : \theta^* = \theta_0$ with contaminated data.

Robustness: Power of the 3-Sign Depth Test for Contaminated Data

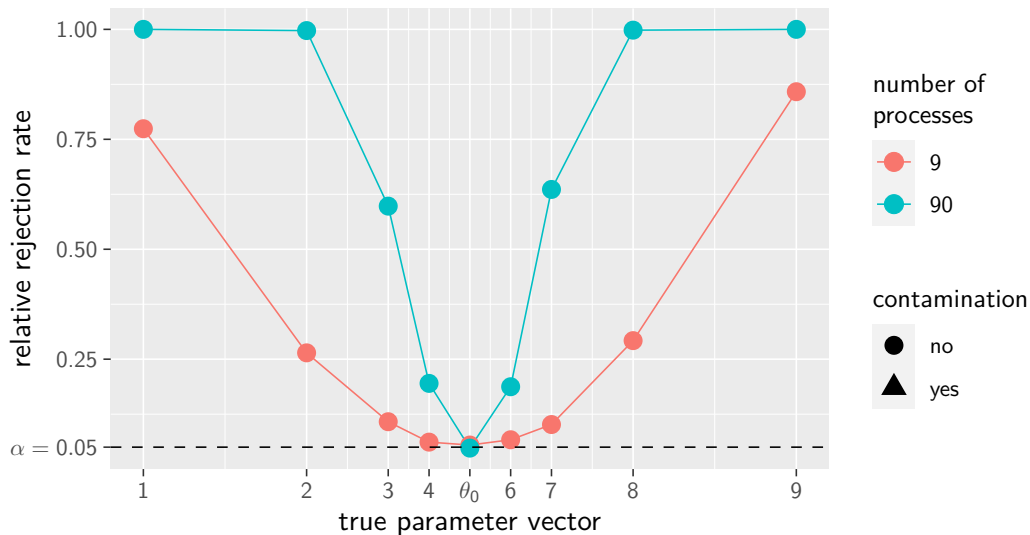


Figure: Power of the 3-sign depth tests for $\mathcal{H}_0 : \theta^* = \theta_0$ with 9 different true parameter vectors along a line through $\theta_0 = (10^{-4}, 3, 1)^\top$. The scaling on the x-axis matches the actual distances.

Robustness: Power of the 3-Sign Depth Test for Contaminated Data

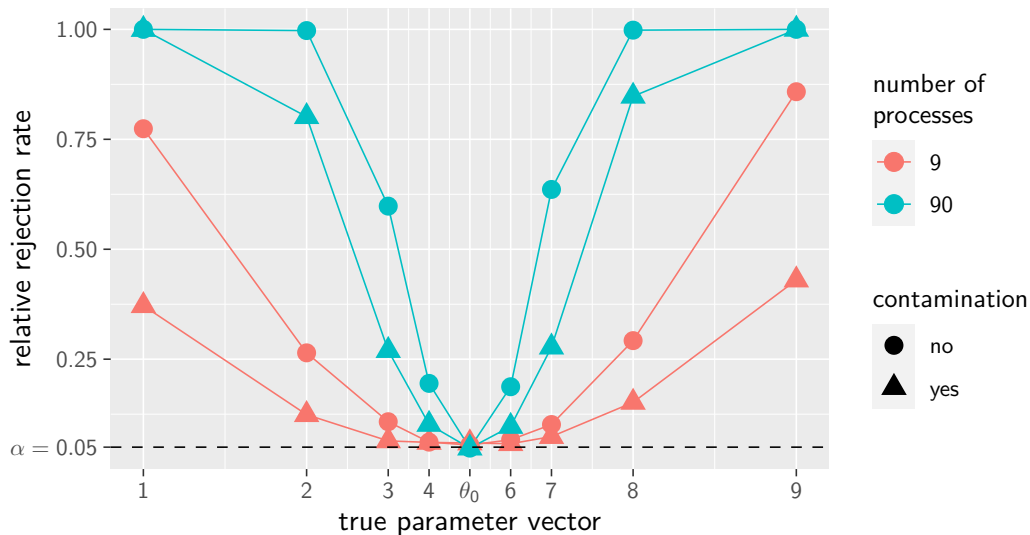


Figure: Power of the 3-sign depth tests for $\mathcal{H}_0 : \theta^* = \theta_0$ with 9 different true parameter vectors along a line through $\theta_0 = (10^{-4}, 3, 1)^\top$. The scaling on the x-axis matches the actual distances.

Real Data Application: Fatigue Tests

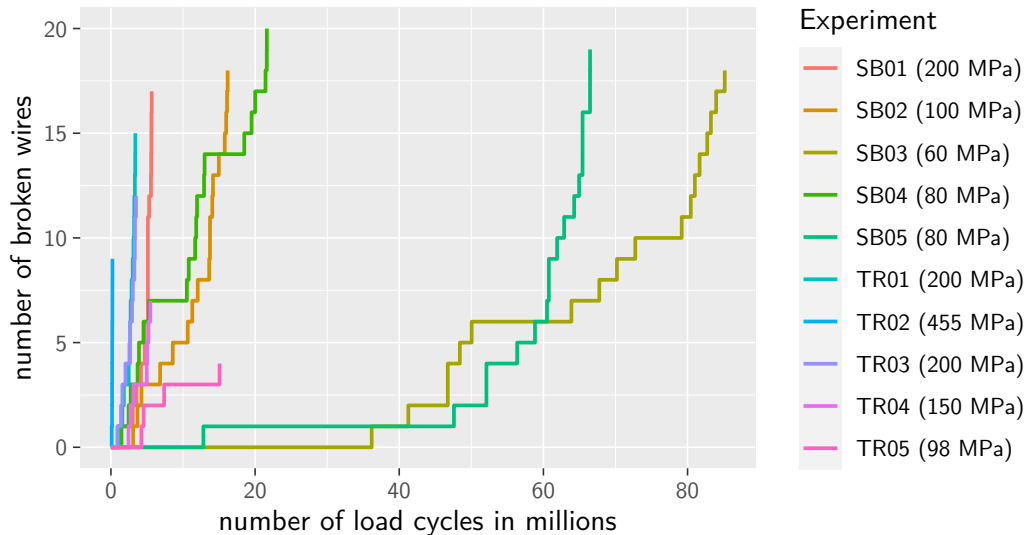


Figure: Results of a series of fatigue tests carried out at TU Dortmund University (Szugat et al. 2016).

Real Data Application: Confidence Set for the True Parameter

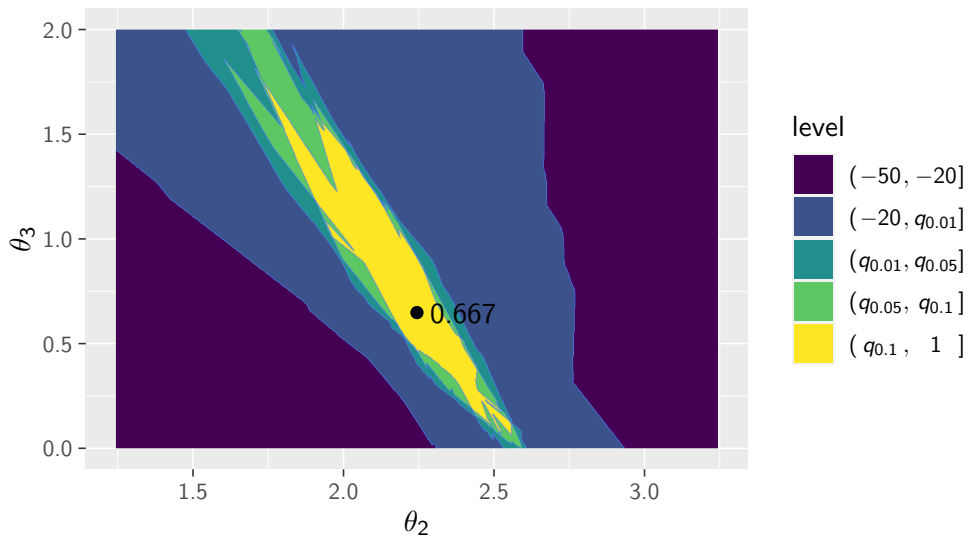


Figure: Two-dimensional slice in θ_2 - θ_3 -direction of the confidence region for the true parameter θ^* based on the fatigue data. The maximum depth of 0.667 is attained at $(\exp(-25.981), 2.244, 0.648)^\top$.

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Intensitätsbasierte Modelle in der Literatur

- Intensitätsbasierte Modelle finden sich in der Literatur seit den 70er Jahren.
 - Multiplikatives Intensitätsmodell (Aalen 1978)
 - Cox-Regressionsmodell (Cox 1972)
 - Relatives Risikoregressionsmodell (Andersen and Gill 1982)
- Anwendung auf Lastumverteilungssysteme hauptsächlich in den letzten zwanzig Jahren.
 - ↪ Kvam and Peña 2005, Balakrishnan, Beutner, and Kamps 2011, Spizzichino 2019, Zhang, Zhao, and Ma 2020, Leckey et al. 2020
- Leckey et al. 2020: Lastumverteilungssystem im relativen Risikoregressionsmodell,

$$h_i^\theta(t \mid T_1^{(j)}, \dots, T_{i-1}^{(j)}) = \theta_1 \left(s_j \frac{1}{1 - (i-1)} \right)^{\theta_2}, \quad i = 1, \dots, c_j,$$

mit zufälligen Kovariaten $s_j > 0$ und $c_j \in \{1, \dots, I\}$.

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initial stress level

Anzahl beobachtbarer Komponentenausfälle

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Erinnerung:
 Auf $\{T_{i-1}^{(j)} < t \leq T_i^{(j)}\}$ gilt:
 $\lambda_{\theta}^{(j)}(t) = h_i^{\theta}(t | T_1^{(j)}, \dots, T_{i-1}^{(j)})$

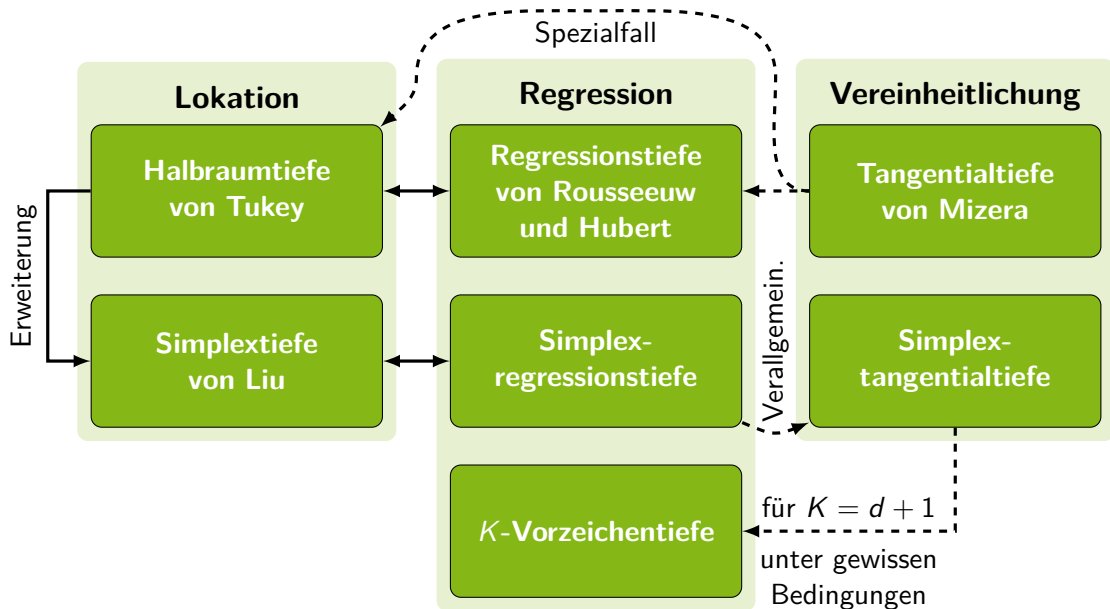
$$h_i^{\theta}(t | T_1^{(j)}, \dots, T_{i-1}^{(j)}) = \theta_1 \left(s_j \frac{1}{l - (i-1)} \right)^{\theta_2}, \quad i = 1, \dots, c_j,$$

mit zufälligen Kovariaten $s_j > 0$ und $c_j \in \{1, \dots, l\}$.

initial stress level

Anzahl beobachtbarer Komponentenausfälle

Übersicht über Zusammenhänge verschiedener Tiefekonzepte



Simulation von Punktprozessen

Algorithmus Simulation eines Punktprozesses mit gegebenen kumulierten bedingten Hazardfunktionen $H_i(\cdot | t_{1:(i-1)}, x)$ durch die Inversionsmethode, s. Daley and Vere-Jones 2003, p. 260. Erfordert, dass die inverse kum. bedingte Hazardfunktion explizit angegeben werden kann.

Eingabe:

$n \in \mathbb{N}$	Anzahl der zu simulierenden Punkte,
\mathbb{P}^X	Verteilung zufälliger Kovariaten,
$t_0 \in \mathbb{R}_+$	Wert von T_0 (determ.), standardmäßig $t_0 = 0$,
$H_i^{-1}(\cdot t_{i-1}, \dots, t_0, x)$	inverse kum. bedingte Hazardfunktion, $i = 1, \dots, n$.

Ausgabe:

$t_{1:n} \in \mathbb{R}_+^n$	Vektor der Realisierungen der Punkte T_1, \dots, T_n .
------------------------------	--

- 1: ziehe Zufallsstichprobe x aus der Kovariaten-Verteilung \mathbb{P}^X
- 2: ziehe u.i.v. Zufallsstichproben y_1, \dots, y_n aus der Exponentialverteilung $\mathcal{E}(1)$ mit $\lambda = 1$
- 3: **for** $i = 1, \dots, n$ **do**
- 4: $t_i \leftarrow H_i^{-1}(y_i | t_{i-1}, \dots, t_0, x)$
- 5: **end for**

Verwendete Parameter in der Simulationsstudie

Nummer des Parametervektors	θ_1^*	θ_2^*	θ_2^*
1	$9.2 \cdot 10^{-5}$	2.92	0.92
2	$9.4 \cdot 10^{-5}$	2.96	0.96
3	$9.8 \cdot 10^{-5}$	2.98	0.98
4	$9.9 \cdot 10^{-5}$	2.99	0.99
5	$10.0 \cdot 10^{-5}$	3.00	1.00
6	$10.1 \cdot 10^{-5}$	3.01	1.01
7	$10.2 \cdot 10^{-5}$	3.02	1.02
8	$10.4 \cdot 10^{-5}$	3.04	1.04
9	$10.8 \cdot 10^{-5}$	3.08	1.08

Table: In der Robustheitsstudie verwendete Parametervektoren. θ_0 ist farblich hervorgehoben.

Kontamination der Daten

- In der Robustheitsstudie wurden zwei Arten von Kontamination untersucht.
- Dazu werden Rohdaten modifiziert, d.h. die u.i.v. Zufallsstichproben y_1, \dots, y_n der $\mathcal{E}(1)$.

1 Tiefe-spezifische Kontamination:

- Kontaminiere Daten durch Erhöhung der Abweichung vom Median $\ln(2)$.
- Für eine Kontamination der i ten Beobachtung, ersetze y_i durch

$$\tilde{y}_i = \max \{2(y_i - \ln(2)) + \ln(2), q_{0.0001}(\mathcal{E}(1))\} .$$

↪ Die Hazardtransformation verändert sich nicht, lediglich die Reihenfolge bzgl. \leq_{acc} .

2 Quantil-basierte Kontamination:

- Kontaminiere Daten durch Ersetzen mit atypisch kleinen oder großen Werten bzgl. $\mathcal{E}(1)$.
- Für eine Kontamination der i ten Beobachtung, ersetze y_i zufällig durch

$$\tilde{y}_i = q_{0.0001}(\mathcal{E}(1)) \quad \text{oder} \quad \tilde{y}_i = q_{0.9999}(\mathcal{E}(1)) .$$

- Im Beispiel aus dem Disputationsvortrag: **40% Quantil-basierte Kontamination.**